## 7. PROPAGATION OF THE OPTICAL FIELD

vs.3.1

PROPAGATION BY PLANE WAVES with circular symmetry PROPAGATION BY SPHERICAL WAVES with circular symmetry THE FAR FIELD

PROPAGATION BY PLANE WAVES

The fundamental problem is the following:

Given the field  $E_1$  at  $z_1$ , calculate the field  $E_2$  at  $z_2$ .

Ignoring evanescent waves  $\underline{S6}_{,}$  the solution of the problem is along the following lines:

- Decompose the field  $\mathsf{E}_1$  into a local plane wave spectrum  $\fbox{S11}$   $\mathsf{A}_1$  according to

$$A_1(k_x,k_y) = E_1(x,y)exp(-jk_xx-jk_yy)dxdy$$
 (7.1)

Propagate all plane waves from z<sub>1</sub> to z<sub>2</sub> by means of the propagator <u>S11</u> H according to

$$A_{2}(k_{x},k_{y}) = H(k_{x},k_{y})A_{1}(k_{x},k_{y})$$
(7.2)

where, in the paraxial approximation S6, H is given by

H (k<sub>x</sub>,k<sub>y</sub>) exp[jk(z<sub>2</sub>-z<sub>1</sub>)]exp[-j(
$$\frac{k_x^2}{2k} + \frac{k_y^2}{2k}$$
)(z<sub>2</sub>-z<sub>1</sub>)] (7.3)

- Sum all plane waves in the propagated spectrum  $\mathsf{A}_2$  to give the field  $\mathsf{E}_2$  according to

$$E_{2}(x,y) = \frac{1}{(2)^{2}} \qquad A_{2}(k_{x},k_{y})exp(jk_{x}x+jk_{y}y)dk_{x}dk_{y} \qquad (7.4)$$

If desired we may use the notation

$$E_1(x,y) = E(x,y,z_1), E_2(x,y) = E(x,y,z_2)$$
 (7.5)

$$A_1(k_x,k_y) = A(K_x,k_y;z_1), \quad A_2(k_x,k_y) = A(K_x,k_y;z_2)$$
(7.6)

The sequence (7.1), (7.2) and (7.4) may be represented in shorthand <u>operator</u> S1 notation:

$$E_2 = F^{-1}H F E_1$$
 (7.7)

Fig. 7.1 is a symbolic representation of the operation (7.7). For simplicity only the X and Z axes are shown.



Fig. 7.1 Schematic representation in two dimensions of the propagation of an optical field by plane waves.

**EX.** 7.1 shows how to calculate the evolution of a Gaussian beam according to (7.7). Examples of numerical calculation using (7.7) may be found in <u>S28</u>.

Circular symmetry

In this case (7.7) should be written

$$E_2 = B^{-1} H B E_1$$
 (7.8)

where B represents the Fourier-Bessel transform. S11

PROPAGATION BY SPHERICAL WAVES

Starting from (7.7), we apply the <u>convolution property</u> <u>S4</u> of the Fourier transform:

$$E_2 = F^{-1}HFE_1 = F^{-1} \{HFE_1\} = F^{-1}H * F^{-1}FE_1 = F^{-1}H * E_1$$

The propagator H being a simple multiplier, we define

$$h = F^{-1} H$$
 (7.10)

so that 7.9 becomes

$$|\mathsf{E}_2 = \mathsf{h} \star \mathsf{E}_1| \tag{7.11}$$

where, with (7.3) and (7.10)

h = F<sup>-1</sup> { exp[jk(z<sub>2</sub>-z<sub>1</sub>)]exp[-j(
$$\frac{k_x^2}{2k}$$
 + $\frac{k_y^2}{2k}$ )(z<sub>2</sub>-z<sub>1</sub>)]} =

 $exp[jk(z_2-z_1)] (1/2)^{2} \times$ 

$$\exp[-j(\frac{k_x^2}{2k} + \frac{k_y^2}{2k})(z_2 - z_1) + jk_xx + jk_yy] dk_x dk_y$$
(7.12)

With the relation **REF.1** 

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$$exp(-p^{2}u^{2} \pm qu) du = \frac{\sqrt{p}}{p}exp(\frac{q^{2}}{4p^{2}})$$
provided p 0 and Re(p<sup>2</sup>) 0. (7.13)

where  $u = k_x$  or  $k_y$ ,  $p^2 = j(z_2 - z_1)/2k$ , and q = jx or jy, we find readily from (7.12) that

$$h = \frac{k}{2} \cdot \frac{1}{j(z_2 - z_1)} \cdot \exp[jk(z_2 - z_1)] \cdot \exp[\frac{jk(x^2 + y^2)}{2(z_2 - z_1)}]$$
(7.14)

With  $z_1 = 0$ ,  $z_2 = z$  and k/2 = we may write (7.14) as

$$h = \frac{1}{j z} \exp[jkz] \exp[\frac{jk(x^2+y^2)}{2z}]$$
(7.15)

which is the form most often encountered in the literature. The function h is sometimes called the <u>impulse response 55</u> of free space.

Applying (7.11) to (7.15) we find

$$E_{2}(x,z) = \frac{1}{j z} \exp[jkz] \times E_{1}(x',y') \exp[\frac{jk[(x-x')^{2}+(y-y')^{2}]}{2z}] dx'dy'$$
(7.16)

**EX.** 7.2 shows an application of (7.16) to the evolution of an elliptical Gaussian beam. Examples of numerical calculation using (7.11) may be found in <u>S28</u>.

With reference to Fig. 7.2 we shall now show that the interpretation of (7.16) is that of the propagation of the field by <u>spherical waves</u> 56.

Let point P<sub>1</sub> of field E<sub>1</sub>, located at x'y', emit a spherical wave with amplitude  $E_1(x',y')dx'dy'$ . The contribution in point P<sub>2</sub>, at x,y, to field E<sub>2</sub> is then given by

dE<sub>2</sub> E<sub>1</sub>(x',y') 
$$\frac{\exp jkr_{12}}{r_{12}}$$
 dx'dy' (7.17)

and hence the total field E<sub>2</sub> is



Fig. 7.2 Propagation of the field by spherical waves.

$$E_{2}(x,y) \qquad E_{1}(x',y') \frac{\exp(jkr_{12})}{r_{12}} dx'dy' \qquad (7.18)$$

The radius  $r_{12}$  is given by

$$r_{12} = \sqrt{z^2 + (x - x')^2 + (y - y')^2}$$
(7.19)

Under conditions of paraxial propagation S6 we assume that the "ray" from P<sub>1</sub> to P<sub>2</sub> lies close to the Z-axis in direction. Under these conditions |(x-x')| << |z| and |(y-y')| << |z|. Eq. (7.19) may then be written as

$$r_{12} z + (x-x')^2/2z + (y-y')^2/2z$$
 (7.20)

We now substitute (7.20) into the exponential phase term  $exp(jkr_{12})$  of (7.18), but the amplitude term  $1/r_{12}$ , not being as sensitive as the phase term, we approximate by 1/z. Eq, (7.18) now becomes

$$E_2(x,z) = \frac{1}{z} \exp[jkz] \times$$

$$E_1(x',y')exp[\frac{jk[(x-x')^2+(y-y')^2]}{2z}] dx'dy'$$
 (7.21)

It is clear that, but for a constant multiplier 1/j, (7.21) is identical to (7.16). Thus the propagation of the field may be interpreted as a propagation by spherical waves. These are emitted by virtual sources — so-called Huyghens sources — P<sub>1</sub>, located upstream to cause the complete field downstream. The Huyghens sources are 90<sup>0</sup> out of phase with the field, as indicated by the factor 1/j.

The basic idea of propagation by spherical waves is due to Huyghens  $\boxed{\texttt{REF. 7.2}}_{i}$  who originated the wave theory of light. Mathematical formulations similar to (7.21) were first derived by Kirchhoff and later by Rayleigh- Sommerfeld. Some of these formalisms have an additional term, called the obliquity factor, multiplying the integrand in (7.21). For the paraxial approximation used here such factors are equal to unity. More information about the Kirchoff and Rayleigh-Sommerfeld theories may be found in  $\boxed{\texttt{REF. 7.3}}$ .

Circular symmetry

We start from (7.8):

$$E_2 = B^{-1}HB E_1$$
 (7.22)

where  $E_1 = E_1(r)$ ,  $E_2 = E_2(r)$ ,  $r = \sqrt{x^2 + y^2}$ , B is the Fourier - Bessel transform S11, and H is the propagator given by

$$H = \exp(jkz)\exp(jk_t^2 z/2k)$$
(7.23)

where we have written  $k_t^2 = k_x + k_y^2$ 

Eq. (7.22) becomes

$$E_2(r) = \exp(jkz) \times$$

$$E_{1}(r')k_{t}r'J_{0}(k_{t}r')J_{0}(k_{t}r)exp(-jk_{t}^{2}z/2k)dk_{t}dr'$$
(7.24)
0 0

We now integrate over  $k_t$  by using the relation REF.1

$$J_p(ax)J_p(bx)exp(-q^2x^2)xdx =$$

$$\frac{1}{2q^2} exp(-\frac{a^2+b^2}{4q^2}) I_p(\frac{ab}{2q^2})$$

where

$$I_p(z) = j^{-p}J_p(jz)$$
, if p is an integer. (7.25)

In our case a = r, b = r',  $q^2 = jz/2k$ , p = 0.

We find

$$E_{2}(r) = \frac{2}{j z} \exp(jkz + \frac{jkr^{2}}{2z}) \times E_{1}(r')r'J_{0}(\frac{krr'}{z})\exp(\frac{jkr'^{2}}{2z})dr'$$
(7.26)

**<u>EX. 7.3</u>** uses (7.26) to show that the field  $E_1(r) = J_0(Kr)$  does not spread by diffraction; it forms a <u>diffraction-free beam</u> <u>S13</u>.

The term multiplying the integral in (7.26) may, to within the paraxial approximation, be written as

 $\frac{2}{j} \frac{\exp(jkR)}{R}$  where R is the distance from the origin to a point

at r in the plane of  $E_2$ , as shown in Fig. 7.3.

The exponential term may be interpreted as a spherical wave originating at the origin. In this interpretation the field  $E_2$  is thus essentially a spherical wave, with a (circularly symmetric) complex amplitude distribution across its wavefront, given by the integral following the spherical wave term.



When z we speak of the far field or Fraunhofer field (Fraunhofer diffraction). The expression for this field is much simplified as we will now show. We start from (7.7):

$$E_{2} = F^{-1} H F E_{1} = F^{-1} H A_{1} =$$

$$\frac{\exp(jkz)}{(2)^{2}} = A_{1}(k_{x},k_{y}) \exp(-j\frac{k_{x}^{2}}{2z}+jkx-j\frac{k_{y}^{2}}{2z}+jky)dk_{x}dk_{y}$$
(7.27)

Completing the squares in  $k_x$  and  $k_y$  in (7.27), we write

$$E_{2} = \frac{\exp(jkz+jk\frac{x^{2}+y^{2}}{2z})}{(2)^{2}} \times A_{1}(k_{x},k_{y}) \exp[-j\frac{z}{2k}(k_{x}-\frac{kx}{z})^{2}]\exp[-j\frac{z}{2k}(k_{y}-\frac{ky}{z})^{2}]dk_{x}dk_{y}$$
- (7.28)

Now, when z , the exponential terms in the argument vary infinitely fast everywhere but in the points  $k_x=kx/z$  and  $k_y=ky/z$ . Thus nowhere but in the infinitesimal neighborhood of these points is there a net contribution from A<sub>1</sub> to the integral <u>S10</u>. This contribution is given by

$$A_{1}(k_{x}=k_{x}/z,k_{y}=k_{y}/z) \times \\ exp[-j\frac{z}{2k}(k_{x}-\frac{kx}{z})^{2}]exp[-j\frac{z}{2k}(k_{y}-\frac{ky}{z})^{2}]dk_{x}dk_{y} = \\ A_{1}(k_{x}=k_{x}/z,k_{y}=k_{y}/z) \times \\ exp[-j\frac{z}{2k}k_{x}^{2}]exp[-j\frac{z}{2k}k_{y}^{2}]dk_{x}dk_{y} = \frac{2k}{jz}$$
(7.29)

by using the relation **REF.1** 

$$\exp(-p^2u^2 \pm qu) du = \frac{\sqrt{p}}{p} \exp(\frac{q^2}{4p^2})$$

provided p = 0 and  $\text{Re}(p^2) = 0$ .

Substituting (7.29) into (7.28), we find finally, for z

$$E_{2} = \frac{1}{j z} \exp(jkz + jk\frac{x^{2}+y^{2}}{2z})A_{1}(k_{x}=kx/z, k_{y}=ky/z)$$

(7.30)

The first two terms in (7.30), as in (7.26), represent a spherical wave centered on the origin. To find the field  $E_2$ , the wavefront of this wave must be multiplied by the complex amplitude distribution  $A_1$ . In other words, the point x,y has an amplitude proportional to the amplitude of the plane wave at  $k_x = kx/z$  and  $k_y = ky/z$ . This is the

plane wave propagating at angles  $k_x/k = x/z$  and '  $k_y/k = y/z$ , i.e the plane wave whose wave vector is directed along the line from the origin to the point P at x,y. Thus, when compensated for by the spherical wave phase term, the far field E  $_2$  at P measures directly the amplitude of the angular plane wave spectrum in the direction OP, where O is the origin and P the observation point. Fig. 7.4 illustrates this interpretation.



FIG. 7.4 The far field as angular spectrum

Because  $A_1 = F E_1$ , eq. (7.30) may also be written as

$$E_{2} = \frac{1}{j z} \exp(jkz + jk\frac{x^{2} + y^{2}}{2z})S (kx/z, ky/z)F E_{1}$$
(7.31)

where S is the symbol exchange operator S1 which indicates that in the Fourier transform F E<sub>1</sub>, k<sub>x</sub> must be replaced by kx/z and k<sub>y</sub> by ky/z. Equation (7.31) is the defining equation of Fraunhofer diffraction S16. The mathematical analysis we have performed to calculate the limiting value of E<sub>2</sub> for z is essentially what is called the stationary phase method S10

EX. 7.1

Propagation of an elliptical Gaussian beam. Plane wave method

For simplicity we assume that  $z_1 = 0$  and  $z_2 = z$ . For an elliptical Gaussian beam the field  $E_1$  at z=0 is given by

$$E(x,y,0) = E_0 \exp(-x^2/w_1^2 - y^2/w_2^2) =$$
  

$$E_0 \exp(-x^2/w_1^2) \exp(-y^2/w_2^2)$$
(7.1.1)

The local plane wave spectrum  $A_1$  at z=0 of this field has been calculated in  $\boxed{EX. 11.1}$ .

$$A(k_x, k_y; 0) = E_0 w_1 w_2 exp(-k_x^2 w_1^2/4 - k_y^2 w_2^2/4)$$
(7.1.2)

The local plane wave spectrum  $\mathsf{A}_2$  at z is found by multiplying  $\mathsf{A}_1$  with

H (k<sub>x</sub>,k<sub>y</sub>) exp[jkz]exp[-j(
$$\frac{k_x^2}{2k} + \frac{k_y^2}{2k}$$
)z] (7.1.3)

so that  $A_2 =$ 

$$A(k_x.k_y;z) = E_0 w_1w_2exp(jkz) \times$$

$$\exp(-k_{x}^{2}w_{1}^{2}/4 - j\frac{k_{x}^{2}}{2k}z) \times$$
$$\exp(-k_{y}^{2}w_{2}^{2}/4 - j\frac{k_{y}^{2}}{2k}z) \qquad (7.1.4)$$

The field  $E_2$  at z may now be found by taking the Fourier transform of (7.1.4):

$$E(x,y,z) = E_0 w_1 w_2 \exp(jkz) \times$$

$$F_x \{ \exp(-k_x^2 w_1^2/4 - j\frac{k_x^2}{2k}z) \} \times$$

$$F_y \{ \exp(-k_y^2 w_2^2/4 - j\frac{k_y^2}{2k}z) \}$$
(7.1.5)

where  $F_{\rm X}$  and  $F_{\rm y}$  are one dimensional inverse Fourier transforms in x and y respectively. We may write

$$E(x,y,z) = E_0 w_1 w_2 exp(jkz) \times$$

$$\frac{1}{2} exp(-k_x^2 w_1^2/4 - j\frac{k_x^2}{2k}z + jk_x x)dk_x \times$$

$$\frac{1}{2} exp(-k_y^2 w_2^2/4 - j\frac{k_y^2}{2k}z + jk_y y)dk_y \qquad (7.1.6)$$

The integrals in (7.1.6) may be solved by application of the following formula  $\boxed{\text{REF.1}}$ 

$$exp(-p^{2}u^{2} \pm qu) du = \frac{\sqrt{p}}{p}exp(\frac{q^{2}}{4p^{2}})$$
provided p 0 and Re(p<sup>2</sup>) 0. (7.1.7)

In our case  $p^2 = w_1^2/4 + jz/2k$  or  $w_2^2/4 + jz/2k$  respectively, and q = jx or jy respectively. Applying (7.1.7) to (7.1.6) we find readily

$$E(x,y,z) = E_0 \exp(jkz) \times \frac{1}{\sqrt{1+j2z/kw_1^2}} \exp\left[\frac{-x^2}{w_1^2(1+j2z/kw_1^2)}\right] \times \frac{1}{\sqrt{1+j2z/kw_2^2}} \exp\left[\frac{-y^2}{w_2^2(1+j2z/kw_2^2)}\right]$$
(7.1.8)

Introducing characteristic lengths,

 $z_{0x} = kw_1^2/2$  and  $z_{0y} = kw_2^2/2$  (7.1.9)

we may write for (7.1.8)

$$E(x,y,z) = E_0 exp(jkz) \times$$

$$\frac{1}{\sqrt{1+jz/z_{0x}}} \exp\left[\frac{-x^{2}}{w_{1}^{2}(1+jz/z_{0x})}\right] \times \frac{1}{\sqrt{1+jz/z_{0y}}} \exp\left[\frac{-y^{2}}{w_{2}^{2}(1+jz/z_{0y})}\right]$$
(7.1.10)

An alternative expression in terms of z-dependent waists, radii of phase curvature and phase angles is given in 56.

Fig. 7.1.1 shows a one dimensional (w<sub>2</sub> = ,  $z_{0y}$  = ) Gaussian in the XZ plane with the amplitude normalized to unity at z=0



Fig. 7.1.1

Ex. 7.2

Propagation of an elliptical Gaussian beam. Spherical waves method

As in Ex. 7.1 the field  $E_1$  is given by

$$E_1(x,y) = E_0 \exp(-x^2/w_0^2) \exp(-y^2/w_0^2)$$
(7.2.1)

Application of (7.16) gives

$$E_{2}(x,z) = \frac{E_{0}}{j z} \exp[jkz] \times \exp[-x'^{2}/w_{1}^{2} - y'^{2}/w_{2}^{2})\exp[\frac{jk[(x-x')^{2} + (y-y')^{2}]}{2z}] dx'dy'$$

or

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$$E_2(x,y) = \frac{E_0}{j z} \exp[jkz + jk(x^2 + y^2)/2z] \times$$

$$exp[-x'^2(1/w_1^2-jk/2z) - jkxx'/2z]dx' \times$$

$$exp[-y'^2(1/w_2^2-jk/2z) - jkyy''/2z]dy'$$
 (7.2.2)

The two integrals may again be solved by application of the relation  $\boxed{\text{REF.1}}$ 

$$exp(-p^{2}u^{2} \pm qu) du = \frac{\sqrt{p}exp(\frac{q^{2}}{4p^{2}})$$
  
provided p 0 and Re(p<sup>2</sup>) 0. (7.2.3)  
with u = x' or y', p<sup>2</sup> = (1/w\_{1}^{2} - jk/2z) or (1/w\_{2}^{2} - jk/2z) and  
q = jkx/2z or jky/2z

After some algebra we find

$$E_{2}(x,y) = E_{0}exp(jkz) \times \frac{1}{\sqrt{1+j2z/kw_{1}^{2}}} exp[\frac{-x^{2}}{w_{1}^{2}(1+j2z/kw_{1}^{2})}] \times \frac{1}{\sqrt{1+j2z/kw_{2}^{2}}} exp[\frac{-y^{2}}{w_{2}^{2}(1+j2z/kw_{2}^{2})}]$$
(7.2.4)

which is identical to (7.1.8) which was calculated by the plane wave propagation method.

EX. 7.3

## Propagation of a diffraction-free beam

If in (7.26) we substitute  $E_2(r') = J_0(Kr')$  where K is a real constant, we find

$$E_{2}(r) = \frac{2}{j z} \exp(jkz + \frac{jkr^{2}}{2z}) \times J_{0}(Kr')r'J_{0}(\frac{krr'}{z})\exp(\frac{jkr'^{2}}{2z})dr'$$
(7.3.1)

We now use the relation Ref.1

$$J_{p}(ax)J_{p}(bx)exp(-q^{2}x^{2})xdx = \frac{1}{2q^{2}}exp(-\frac{a^{2}+b^{2}}{4q^{2}})I_{p}(\frac{ab}{2q^{2}})$$
(7.3.2)

where

$$I_p(z) = j^{-p}J_p(jz), \text{ if } p \text{ is an integer.}$$
(7.3.3)

In our case x = r', p = 0, a = K, b = kr/z, and  $q^2 = -jk/2z$ 

By substituting these values into (7.3.2) we find for the integral the value

$$\frac{jz}{2} \exp[-j\frac{z}{2k} (K^2 + \frac{k^2r^2}{z^2})]J_0(Kr)$$

and hence for E<sub>2</sub>:

$$E_2(r) = \exp[j(k - \frac{K^2}{2k})z] J_0(Kr)$$
(7.3.4)

Hence  $|E_2(r)| = |E_1(r)| = |J_0(Kr)|$ , and the beam is diffraction-free.

REFERENCES

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