Lecture 4: Undamped Free Vibration

Reading materials: Section 2.1

1. Introduction

• The terminology of "Free Vibration" is used for the study of natural vibration modes in the absence external loading.

• Free vibration solution of multi-degree of freedom systems follows procedure similar to the one used for a single degree of freedom system.

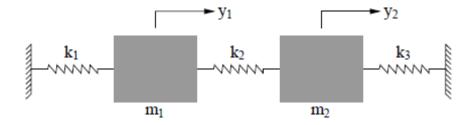
• The number of DOFs of the system is the number of masses in the system multiplying the number of possible types of motion of each mass.

Generally, the number of equations of motion is the number of DOFs. They are in form of *coupled differential equations*. In other words, each equation involves all the DOFs/coordinates.

• All differential equations for the system must be solved simultaneously.

• The matrix notation is used to indicate the system of equations for a general case.

2. A two DOFs spring-mass system



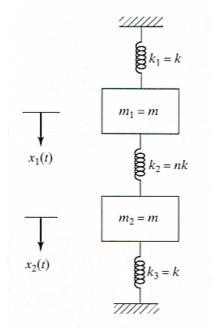
$$\omega_{1}^{2} = \frac{k_{2}m_{1} + k_{3}m_{1} + k_{1}m_{2} + k_{2}m_{2} - \sqrt{\left(-k_{2}m_{1} - k_{3}m_{1} - k_{1}m_{2} - k_{2}m_{2}\right)^{2} - 4\left(k_{1}k_{2} + k_{3}k_{2} + k_{1}k_{3}\right)m_{1}m_{2}}{2m_{1}m_{2}}$$

$$\omega_{2}^{2} = \frac{k_{2}m_{1} + k_{3}m_{1} + k_{1}m_{2} + k_{2}m_{2} + \sqrt{\left(-k_{2}m_{1} - k_{3}m_{1} - k_{1}m_{2} - k_{2}m_{2}\right)^{2} - 4\left(k_{1}k_{2} + k_{3}k_{2} + k_{1}k_{3}\right)m_{1}m_{2}}{2m_{1}m_{2}}$$

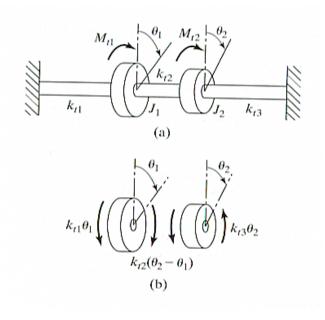
3. Examples:

Compute natural frequencies and mode shapes for a two DOF spring-mass system as shown in above with $m_1=9$; $m_2=1$; $k_1=38$; $k_2=2$; $k_3=3$

• Find the natural frequencies and mode shapes of a spring-mass system, shown below, which is constrained to move in the vertical direction only. (n=1)



4. Torsional System



5. Frequencies and mode shapes using standard eigenvalue problem

• If mass matrix is non-singular, the frequency equation can easily be expressed in the form of a standard egienvalue problem.

$$[\boldsymbol{k} - \lambda \boldsymbol{m}] \boldsymbol{\phi} = \begin{bmatrix} \boldsymbol{m}^{-1} \boldsymbol{k} - \lambda \boldsymbol{m}^{-1} \boldsymbol{m} \end{bmatrix} \boldsymbol{\phi} = \boldsymbol{0} \implies \begin{bmatrix} \boldsymbol{m}^{-1} \boldsymbol{k} - \lambda \boldsymbol{I} \end{bmatrix} \boldsymbol{\phi} = \boldsymbol{0}$$

• The above is a standard eigenvalue problem. The mode shapes are the eigenvectors while the frequencies are the square roots of the egienvalues.

Another efficient way for larger systems.

Sector Example: Compute natural frequencies and mode shapes for a two DOF spring-mass system as shown in above with $m_1=9$; $m_2=1$; $k_1=38$; $k_2=2$; $k_3=3$

- 6. Exact solutions based on the given initial conditions
- General solutions of the free vibration:

$$y_1(t) = \left(a e^{i\omega_1 t} + b e^{-i\omega_1 t}\right) \phi_1^{(1)} + \left(c e^{i\omega_2 t} + d e^{-i\omega_2 t}\right) \phi_1^{(2)}$$
$$y_2(t) = \left(a e^{i\omega_1 t} + b e^{-i\omega_1 t}\right) \phi_2^{(1)} + \left(c e^{i\omega_2 t} + d e^{-i\omega_2 t}\right) \phi_2^{(2)}$$

in matrix form

$$\mathbf{y}(t) = \left(a \, e^{i \,\omega_1 \, t} + b \, e^{-i \,\omega_1 \, t}\right) \boldsymbol{\phi}^{(1)} + \left(c \, e^{i \,\omega_2 \, t} + d \, e^{-i \,\omega_2 \, t}\right) \boldsymbol{\phi}^{(2)}$$

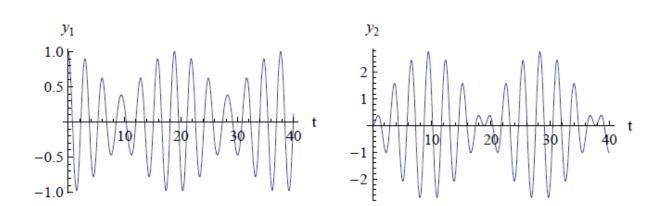
or

$$\mathbf{y}(t) = \sum_{m} (A_m \cos \omega_m t + B_m \sin \omega_m t) \boldsymbol{\phi}^{(m)}$$

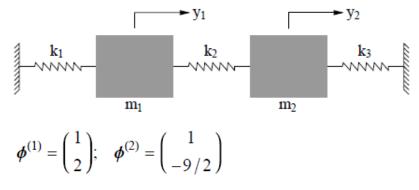
• The unknown coefficients can be determined via initial conditions.

• Example:

Compute free vibration solution of a two DOF spring-mass system as shown in above with $m_1=9$; $m_2=1$; $k_1=38$; $k_2=2$; $k_3=3$ and the following initial conditions: $y_1(0) = 1$; $y_2(0) = 0$; $v_1(0) = 0$; $v_2(0) = 0$



7. Interpretation of mode shapes



• In the first mode shape the two masses are moving in the same direction.

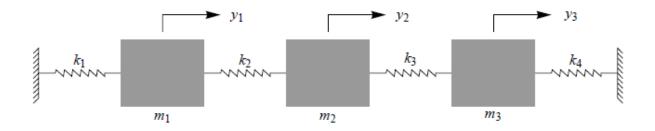
• The movement of the first mass is smaller than the second mass in this mode because the first mass is attached to a stiffer spring.

• In the second mode shape the two masses are moving in the opposite directions. The movement of the first mass is also smaller than the second mass.

There are only two possibilities of independent motion of this two DOF system indicated by those two mode shapes. Any other motion can be described in terms of a linear combination of these two modes. For example:

$$\begin{pmatrix} 1 \\ 0 \end{pmatrix} = \frac{9}{13} \not 0^{(1)} + \frac{4}{13} \not 0^{(2)}$$

8. Example: free vibration solution of the following three DOF system (Optional)



 $m_{1} = m_{2} = m_{3} = 4; \quad k_{1} = k_{2} = k_{3} = 5; \quad k_{4} = 10$ $\begin{pmatrix} y_{1}(0) \\ y_{2}(0) \\ y_{3}(0) \end{pmatrix} = \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix}; \quad \begin{pmatrix} \dot{y}_{1}(0) \\ \dot{y}_{2}(0) \\ \dot{y}_{3}(0) \end{pmatrix} = \begin{pmatrix} 1 \\ 0 \\ 1 \end{pmatrix}$

$$\omega_{1} = \sqrt{\lambda_{1}} = 0.970194; \qquad \omega_{2} = \sqrt{\lambda_{2}} = 1.74823; \qquad \omega_{3} = \sqrt{\lambda_{3}} = 2.18001$$

$$\phi^{(1)} = U^{-1}\overline{\phi}^{(1)} = \begin{pmatrix} 0.295505\\ 0.368488\\ 0.163993 \end{pmatrix}; \qquad \phi^{(2)} = U^{-1}\overline{\phi}^{(2)} = \begin{pmatrix} 0.368488\\ -0.163993\\ -0.295505 \end{pmatrix};$$

$$\phi^{(3)} = U^{-1}\overline{\phi}^{(3)} = \begin{pmatrix} 0.163993\\ -0.295505\\ 0.368488 \end{pmatrix}$$