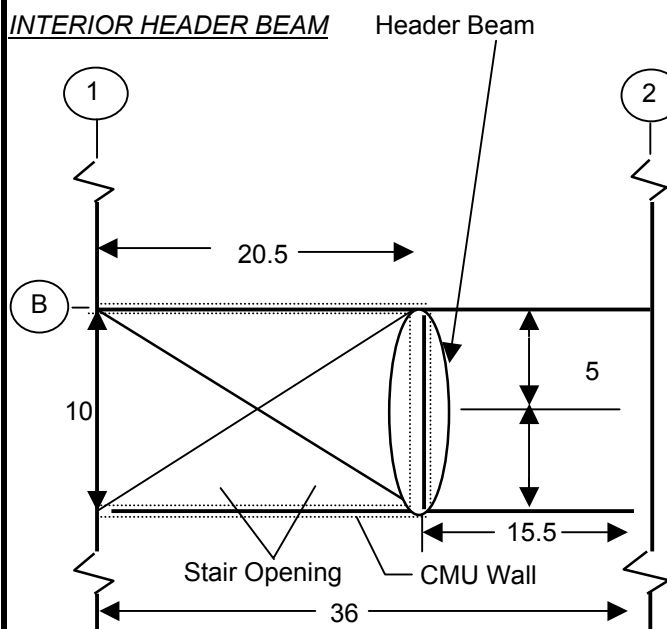
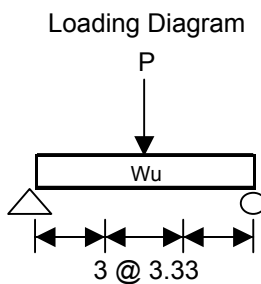


INTERIOR HEADER BEAM SELECTION - Bay length = 36 ft. (stairwell)

INTERIOR HEADER BEAM



Total Bay Length =	36	(ft)	
Total Bay Width =	10	(ft)	
Fill Beam Fy =	50	(ksi)	
DL _{CMU wall} =	51.0	(lb/ft ²)	Tributary width
DL _{beam} =	2.5	(lb/ft ²)	0.7 (ft)
LL _{stairs} =	100.0	(lb/ft ²)	18.0 (ft)
DL _{joist} =	56.5	(lb/ft ²)	10.3 (ft)
LL _{joist} =	80.0	(lb/ft ²)	
WDL _{joist} =	282.5	(lb/ft)	
WLL _{joist} =	400	(lb/ft)	
PDL _{joist} =	2189.4	(lb)	
PLL _{joist} =	3100	(lb)	
W _{DL(CMU)} =		(lb/ft)	
W _{DL(beam)} =		(lb/ft)	
W _{LL(stair)} =		(lb/ft)	



Factored Load = Wu =		(lb/ft)	
Factored Max. Moment (Mu) =		(k-ft)	← distributed loads
factored load = P =		(lb)	
Factored Max. Moment (Mu) =		(k-ft)	← 2 equal, concentrated symmetrically placed
TOTAL Factored Max. Moment (Mu) =		(k-ft)	

SELECT SECTION

LRFD p5-40 - Choose
 Beam Weight (k/ft)

Mu =		(k-ft)
φMp =		(k-ft)
	←	φMp > Mu ?

CHECK LOCAL CONDITIONS

b _t / 2 t _f (LRFD p1-29) =	
λ _p = 65 / Fy ⁵ =	
	← λ _p > b _t /2t _f ?

CHECK WEB

h / tw (LRFD p1-29) =	
λ _p = 640 / Fy ⁵ =	
	← λ _p > h/tw ?

Red font indicates user input

INTERIOR HEADER BEAM SELECTION - (continued)

CHECK SHEAR CAPACITY

$$V_u = W_u * L / 2 + P = \text{[redacted]}$$

$$\phi V_n = \phi_v (0.6 F_{yw}) A_w \quad (F_{yw} = \text{yield strength of web}) = \text{[redacted]} \quad (\phi_v = .9)$$

$$A_w = d * t_w \quad (\text{LRFD p1-28}) = \text{[redacted]}$$

$$d = \text{[redacted]}, \quad t_w = \text{[redacted]}$$

← $\phi V_n > V_u ?$

LIVE LOAD DEFLECTION CHECK

$$\Delta = L / 360 = \text{[redacted]} \quad (\text{in}) - \text{LIMIT}$$

$$\Delta (w_u) = (5 * w_{LL} * L^4) / (384 * E * I) = \text{[redacted]}$$

$$\Delta (P) = ((P * a) / (24 * E * I)) / (3 * L^2 - 4 * a^2) = \text{[redacted]}$$

$$I \text{ (moment of inertia about x-x axis, LRFD)} = \text{[redacted]}$$

← $\Delta_{limit} > \Delta_{LL} ?$

NOTE -- The header beam has a combination of 4 distributed loads and 2 point loads. The distributed loads are the CMU dead load, the floor dead load (same for floor and stairwell - conservative), the stair live load and floor live load. Since there are only 2 joists, these are treated as point loads. These point loads are determined by a simple analysis of the loading on each joist and determining their reactions.

Cost Per Ton **1950** (\$)
 Total Cost [redacted]

In this case, deflection controls

Red font indicates user input

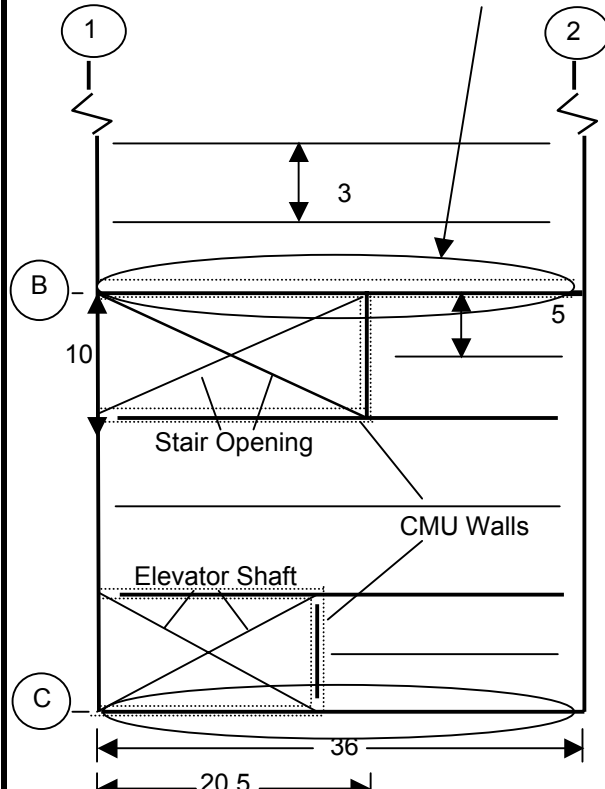
SECTION OK

INTERIOR FLOOR FILL BEAM SELECTION - Bay length = 36 ft. (stairwell)

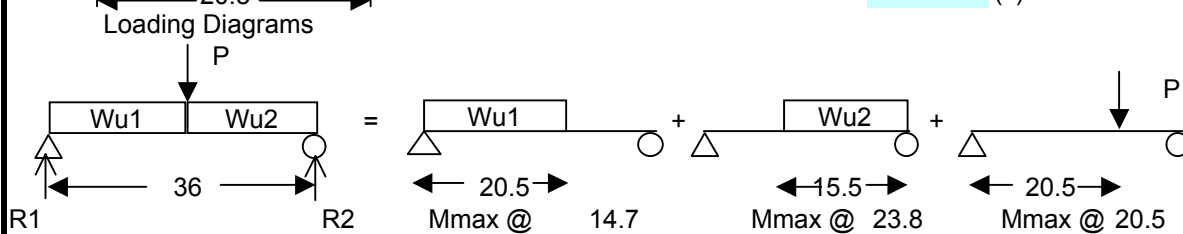
INTERIOR FLOOR FILL BEAM

Note: Shear studs along the beams that are part of the lateral load-resisting truss are necessary to transfer the lateral loads from the floor diaphragms to the resisting members. This is outside the scope of this case study.

Interior Floor Fill Beam



Total Bay Length =	36	(ft)	
Total Bay Width =	30	(ft)	
Fill Beam Fy =	50	(ksi)	
DL _{CMU wall} =	51.0	(lb/ft ²)	Tributary width 0.7 (ft)
DL _{beam1} =	59.0	(lb/ft ²)	4.0 (ft)
DL _{beam2} =	59.0	(lb/ft ²)	1.5 (ft)
LL _{stairs} =	100.0	(lb/ft ²)	5.0 (ft)
LL _{office1} =	80.0	(lb/ft ²)	1.5 (ft)
LL _{office2} =	80.0	(lb/ft ²)	4.0 (ft)
WDL _{CMU wall} =	34	(lb/ft)	
WDL _{beam1} =	236.0	(lb/ft)	
WDL _{beam2} =	88.5	(lb/ft)	
WLL _{stairs} =	500	(lb/ft)	
WLL _{office1} =	120	(lb/ft)	
WLL _{office2} =	320	(lb/ft)	
PDL _{header beam} =	2189.4	(lb)	
PLL _{header beam} =	3100.0	(lb)	
Wu1 =		(k/ft)	
Wu2 =		(k/ft)	
P =		(k)	



	Moment by superposition (k-ft)			
	at 14.7'	at 18'	at 20.5'	at 23.8'
Wu1				
Wu2				
P				
Total				

Mmax = (K-ft)

Red font indicates user input

	Shear by Superposition (k)	
	R1	R2
Wu1		
Wu2		
P		
Total		

INTERIOR FLOOR FILL BEAM (continued)

SELECT SECTION

LRFD p5-40 - Choose

Beam Weight (k/ft)

Mu = []

φMp = []

<than 85 plf assmd, sheet6

(k-ft)

(k-ft)

← φMp > Mu ?

CHECK LOCAL CONDITIONS

$b_f / 2 t_f$ (LRFD p1-17) = []

$\lambda_p = 65 / F_y^5 =$ []

← λp > bf/2tf ?

CHECK WEB

h / t_w (LRFD p1-17) = []

$\lambda_p = 640 / F_y^5 =$ []

← λp > h/tw ?

CHECK SHEAR CAPACITY

$V_u = W_u * L / 2 - P * a / L =$ []

$\phi V_n = \phi_v (0.6 F_{yw}) A_w$ (F_{yw} = yield strength of web) = [] ($\phi_v = .9$)

$A_w = d * t_w$ (LRFD p1-16) = []

d = [], $t_w =$ []

← φVn > Vu ?

LIVE LOAD DEFLECTION CHECK

$\Delta_{max} = L / 360 =$ [] (in) - LIMIT

Deflection at Mmax :

$\Delta(P) = (P * b * x) * (L^2 - b^2 - x^2) / (6 * E * I * L) =$ []

$\Delta(Wu1) = W * a^2 * (L - x) * (4 * L * x - 2 * x^2 - a^2) / (24 * E * I * L) =$ []

$\Delta(Wu2) = W * a^2 * (L - x) * (4 * L * x - 2 * x^2 - a^2) / (24 * E * I * L) =$ []

I (moment of inertia about x-x axis, LRFD) = []

(in) - ΔLL

(in⁴)

← Δlimit > ΔLL?

NOTE -- The fill-beam has a combination of several uniform and partially distributed loads and 2 concentrated loads. The dead load for the floor and stair is uniformly distributed as well as the floor live load. The CMU dead load is only partially distributed along the length of the member PLUS 1/2 of the distance along the header (the fill beam picks up half this load). This fill-beam also picks up 2 partially distributed live loads for the floor and stair. There is one concentrated dead and live load at the point where the header frames into the fill beam.

SECTION OK

Cost Per Ton

1950

(\$)

Total Cost

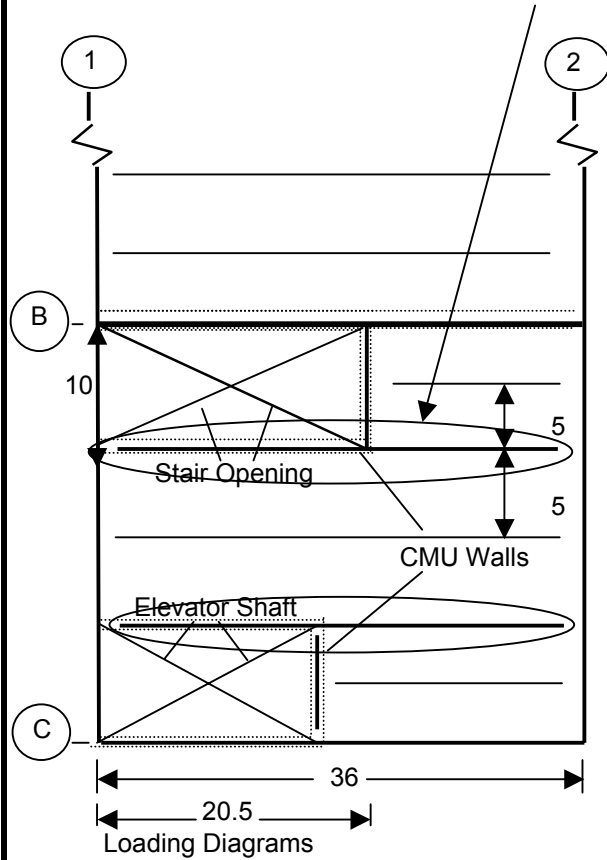
In this case, deflection controls

Red font indicates user input

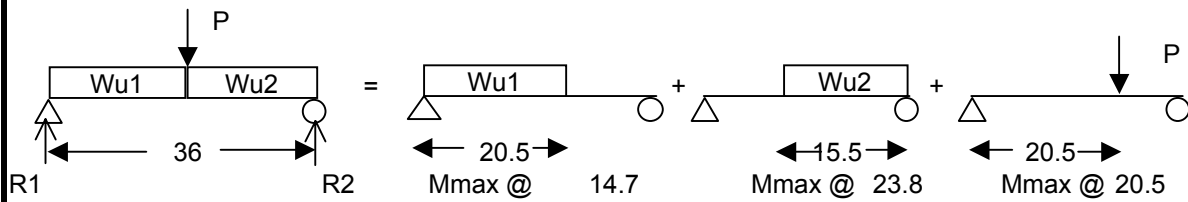
INTERIOR FLOOR FILL BEAM SELECTION - Bay length = 36 ft. (stairwell)

INTERIOR FLOOR FILL BEAM

Interior Floor Fill Beam



Total Bay Length =	36	(ft)	
Total Bay Width =	30	(ft)	
Fill Beam Fy =	50	(ksi)	
DL _{CMU wall} =	51.0	(lb/ft ²)	tributary width 0.7 (ft)
DL _{beam1} =	59.0	(lb/ft ²)	5.0 (ft)
DL _{beam2} =	59.0	(lb/ft ²)	2.5 (ft)
LL _{stairs} =	100.0	(lb/ft ²)	5.0 (ft)
LL _{office1} =	80.0	(lb/ft ²)	2.5 (ft)
LL _{office2} =	80.0	(lb/ft ²)	5.0 (ft)
WDL _{CMU wall} =	34	(lb/ft)	
WDL _{beam1} =	295.0	(lb/ft)	
WDL _{beam2} =	147.5	(lb/ft)	
WLL _{stairs} =	500	(lb/ft)	
WLL _{office1} =	200	(lb/ft)	
WLL _{office2} =	400	(lb/ft)	
PDL _{header beam} =	2189.4	(lb)	
PLL _{header beam} =	3100.0	(lb)	
Wu1 =		(k/ft)	
Wu2 =		(k/ft)	
P =		(k)	



Moment by superposition (k-ft)				
	at 14.7'	at 18'	at 20.5'	at 23.8'
Wu1				
Wu2				
P				
Total				

Shear by Superposition (k)		
	R1	R2
Wu1		
Wu2		
P		
Total		

Mmax = (K-ft)

Red font indicates user input

INTERIOR FLOOR FILL BEAM (continued)

SELECT SECTION

LRFD p5-40 - Choose

Beam Weight (k/ft)

Mu = []

φMp = []

<than 85 plf assmd, sheet6

(k-ft)

(k-ft)

← φMp > Mu ?

CHECK LOCAL CONDITIONS

b_f / 2 t_f (LRFD p1-17) = []

λ_p = 65 / F_y⁵ = []

← λ_p > b_f/2t_f ?

CHECK WEB

h / t_w (LRFD p1-17) = []

λ_p = 640 / F_y⁵ = []

← λ_p > h/t_w ?

CHECK SHEAR CAPACITY

V_u = W_u * L / 2 P*a/L = []

φV_n = φ_v (0.6 F_{yw}) A_w (F_{yw} = yield strength of web) = []

(φ_v = .9)

A_w = d * t_w (LRFD p1-16) = []

d = [], t_w = []

← φV_n > V_u ?

LIVE LOAD DEFLECTION CHECK

Δ max = L / 360 = [] (in) - LIMIT

Deflection at Mmax :

Δ(P) = (P*b*x)(L² - b² - x²) / (6*E*I*L) = []

Δ(Wu1) = W*a² *(L-x)(4*L*x - 2*x² - a²) / (24* E * I * L) = []

Δ(Wu2) = W*a² *(L-x)(4*L*x - 2*x² - a²) / (24* E * I * L) = []

I (moment of inertia about x-x axis, LRFD) = []

(in) - Δ_{LL}

(in⁴)

← Δ_{limit} > Δ_{LL} ?

SECTION OK

NOTE -- The fill-beam has a combination of several uniform and partially distributed loads and 2 concentrated loads. The dead load for the floor and stair is uniformly distributed as well as the floor live load. The CMU dead load is only partially distributed along the length of the member PLUS 1/2 of the distance along the header (the fill beam picks up half this load). This fill-beam also picks up 2 partially distributed live loads for the floor and stair. There is one concentrated dead and live load at the point where the header frames into the fill beam.

SECTION OK

Cost Per Ton
 Total Cost

1950

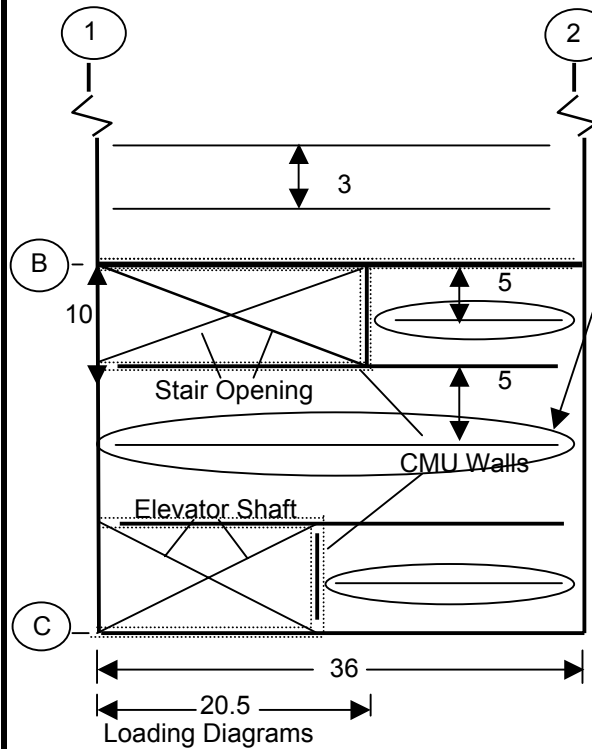
(\$)

In this case, deflection controls

Red font indicates user input

INTERIOR FLOOR FILL BEAM SELECTION - Bay length = 36 ft. (stairwell)

INTERIOR FLOOR FILL BEAM



Interior Floor Fill Beam
 (Braces bottom flange of girder in lateral resisting truss)

Spacing = 5 (ft)
 DL = 61.0 (lb/ft²)
 LL = 80.0 (lb/ft²)
 W_{DL} = (lb/ft)
 W_{LL} = (lb/ft)
 Applied Load - W_u = (lb/ft)

SELECT SECTION

LRFD p.5-48 - Choose
 Beam Weight (k/ft)

M_u = (k-ft) > 11 plf assumed, add Wt.
 φM_p = (k-ft)
 φM_p > M_u ?

LIVE LOAD DEFLECTION CHECK

$\Delta = L / 360 =$ (in) - LIMIT
 $\Delta = (5 \cdot W_{LL} \cdot L^4) / (384 \cdot E \cdot I) =$ (in) - Δ_{LL}
 I (moment of inertia about x-x axis, LRFD p.5-48) = (in⁴)
 Δ_{limit} > Δ_{LL} ?

Note: Fill beam for this bay will be the same on the 2nd and 3rd floors. On the 4th and roof use interior fill beams determined previously for this bracing beam. The beam is necessary to laterally brace the W 24 x 68 framing beam. The beam is part of the North/South lateral load-resisting truss. A plate is added to brace the bottom flange against buckling out-of-plane.

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