

Equations and constants you may (or may not) find useful:

$$f^* = \phi$$

$$I_a = 0.2S$$

$$Q(t) = Q(t_0)K^{(t-t_0)}$$

$$t_l = 0.6t_c$$

$$Q_p = \frac{CA}{T_p}$$

$$F(x) = \exp\left[-\exp\left(-\frac{x-b}{a}\right)\right]$$

$$a = \frac{\sqrt{6}\sigma}{\pi}$$

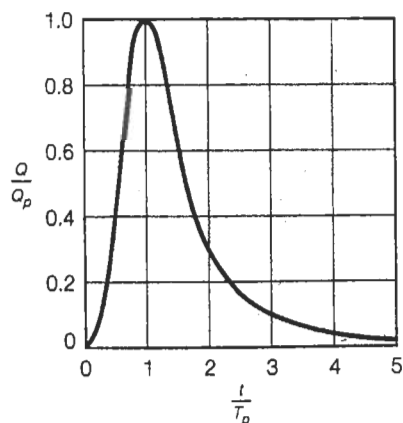
$$y = -\ln(-\ln(1-p))$$

$$T = \frac{1}{p}$$

$$1 \text{ in} = 25.4 \text{ mm}$$

$$1 \text{ mi}^2 = 640 \text{ ac}$$

$$1 \text{ hr} = 3600 \text{ s}$$



(a) Dimensionless Unit Hydrograph

$$P_e = \frac{(P - I_a)^2}{P - I_a + S}$$

$$S = \frac{1000}{CN} - 10$$

$$V_d = Ar_d$$

$$T_p = \frac{t_r}{2} + t_l$$

$$R_{k+1} = \alpha R_k + \frac{(1+\alpha)}{2}(Q_{k+1} - Q_k)$$

$$q(p) = b - a \ln(-\ln(1-p))$$

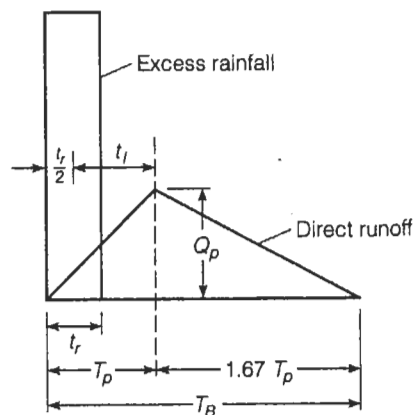
$$b = \mu - 0.5772a$$

$$P(X \geq x_m) = \frac{m}{N+1}$$

$$1 \text{ ft} = 12 \text{ in}$$

$$1 \text{ acre} = 43560 \text{ ft}^2$$

$$1 \text{ day} = 86400 \text{ s}$$



(b) Triangular Unit Hydrograph

(25) 1. Miscellaneous

- 6 a) The SCS runoff curve number (CN) is determined based on the following three factors:

land use/land cover

hydrologic soil group

antecedent moisture condition

- 5 b) The baseflow today is 50 cfs. The baseflow one week ago was 67 cfs. Assuming this baseflow-only period continues, the estimated baseflow one week from today is 37.3 cfs.

$$Q(t) = Q(t_0)K^{(t-t_0)} \quad \text{In one week}$$
$$50 = 67K^7 \quad Q(7) = 50K^7$$
$$\therefore K^7 = \frac{50}{67} \quad = 50\left(\frac{50}{67}\right)$$
$$= 37.3$$

- c) List three (unique) properties of a unit hydrograph:

P_e is 1 unit (in or cm)

$P_e = 1 = i_e t_r$

r_d is 1 unit ($P_e = r_d$)

$V_d = A r_d = A(1 \text{ unit})$

- d) Define the time of concentration (t_c):

travel time from the farthest point (hydraulically) to the basin outlet

- e) List the two assumptions made in flood frequency analysis:

Independence - flood data are a random sample

Stationarity - flood distribution does not change with time

(25) 2. Streamflow Prediction

Predict the direct runoff hydrograph for the Mays Creek watershed (1.16 mi²). The storm rainfall (P) and the 2-hour unit hydrograph for the watershed are shown below. The SCS curve number (CN) for the watershed at the time of the storm is 80.

Time (hours)	P (inch)	ΣP (in)	ΣP_e (in)	P_e (in)	Time (hours)	2-hour UH (cfs)
0		0	0	0	0	0
2	0.2	0.2	0	0	1	150
4	2.6	2.8	1.1	1.1	2	300
6	1.4	4.2	2.2	1.1	3	200
					4	100
					5	0

Use this information to determine the following:

22 a) The direct runoff hydrograph (in cfs). *CLEARLY INDICATE YOUR ANSWER.*

b) The peak discharge of the direct runoff hydrograph is 440 cfs at time 6 hour.

Use SCS method:

$$S = \frac{1000}{CN} - 10 = \frac{1000}{80} - 10 = 2.5''$$

$$I_a = 0.2S = 0.2(2.5'') = 0.5''$$

$$\therefore P_e = \frac{(P - I_a)^2}{P - I_a + S} = \frac{(P - 0.5)^2}{P - 0.5 + 2.5} = \frac{(P - 0.5)^2}{P + 2}, \quad P \geq I_a$$

$$\text{at } t = 2 \text{ hr } P = 0.2 < I_a \rightarrow P_e = 0$$

$$\text{at } t = 4 \text{ hr } P = 2.8, \quad P_e = \frac{(2.8 - 0.5)^2}{2.8 + 2} = 1.10''$$

$$\text{at } t = 6 \text{ hr } P = 4.2, \quad P_e = \frac{(4.2 - 0.5)^2}{4.2 + 2} = 2.21'' \sim 2.2''$$

Need 2-hr UH:

t	2-hr UH (cfs)	$1.1 \times \text{UH}$ <u>DBH₁</u>	$1.1 \times \text{UH}$ <u>DBH₂</u>	(a) <u>ΣDBH</u>
0	0	--	--	--
1	150	--	--	--
2	300	0	--	0
3	200	165	--	165
4	100	330 +	0 =	330
5	0	220	165	385
6		110	330	440 ← Q_p at $t = 6 \text{ hr}$
7		0	220	220
8			110	110
9			0	0

(25) 3. Hydrograph Analysis

Shown below are the storm rainfall (P) and resulting streamflow (Q) for a flood event on a 12.4 mi^2 watershed.

Time (hour)	P (in)	Q (cfs)	ϕ_b (cfs)	DRH (cfs)	i (in/hr)
0		300	300	--	
3	0.60	300		0	0.20
6	2.16	1200		900	0.72
9	1.89	1500		1200	0.63
12	1.11	1200		900	0.37
15		900		600	
18		300		0	
21		300	300	--	

$\Sigma 3600 \text{ cfs}$

Use hydrograph analysis techniques, with the horizontal line method for baseflow separation, to answer the following:

- 1) a) The depth of direct runoff (r_d) is 1.35 inches.
 b) The rainfall excess (P_e) hyetograph (in inches). *CLEARLY INDICATE YOUR ANSWER.*
 3 c) The effective duration (t_e) is 6 hours.

$$a) V_d = (\Sigma \text{DRH}) \Delta t = (3600 \text{ cfs})(3 \text{ hr}) = 10,800 \text{ cfs-hr}$$

$$r_d = \frac{V_d}{A} = \frac{10,800 \frac{\text{ft}^3}{\text{s}} \cdot \text{hr} (3600 \text{ s/hr})(12^{17} \text{ ft}^2)}{12.4 (640 \times 43560 \text{ ft}^2)} = 1.35 \text{ in}$$

b) Assume $\phi > 0.63$, then

$$r_d = 1.35 = (0.72 - \phi)(3)$$

$$\phi = 0.72 - \left(\frac{1.35}{3}\right) = 0.27 \text{ in/hr} < 0.63 \text{ in/hr (Not OK)}$$

Assume $0.37 \leq \phi \leq 0.63 \text{ in/hr}$, then

$$r_d = 1.35 \text{ in} = (0.72 - \phi)(3) + (0.63 - \phi)(3)$$

$$2\phi = 0.72 + 0.63 - \left(\frac{1.35}{3}\right) = 0.90$$

$$\phi = 0.45 \text{ in/hr [OK]}$$

$$L_e = L - \phi \quad L > \phi$$

Hence,

t	i (in/hr)	L_e (in/hr)	P_e (in)
0	0.20	--	0
3	0.72	0.27	0.81
6	0.63	0.18	0.54
9	0.37	--	0
12			

(b)

} 6-hr

$\Sigma 1.35 \quad \checkmark$

(25) 4. Flood Frequency Analysis Using Sample Data

Recent record flooding on the Big Bad River has motivated the town of Burgeville to consider building a flood levee. A nearby streamgauge on the river has a 60-year record. The ranked sample of annual maximum peak discharges and the sample moments are:

Rank	Peak Discharge (cfs)
1	5850
2	4120
3	4000
..	..
..	..
58	410
59	390
60	200

$$\bar{x} = 1704 \text{ cfs}$$

$$\hat{\sigma} = 1112 \text{ cfs}$$

$$\hat{a} = \frac{\sqrt{6}}{\pi} \hat{\sigma} = \frac{\sqrt{6}}{\pi} (1112)$$

$$= 867.0 \text{ cfs}$$

$$\hat{b} = \bar{x} - 0.5772 \hat{a}$$

$$= 1704 - 0.5772(867)$$

$$= 1203.6 \text{ cfs}$$

- a) Assume that a peak discharge of 4000 cfs or greater is a *damaging flood event*. The estimated return period for a damaging flood is 25.7 years based on a fitted EVI distribution (parametric method) and 20.3 years based on its plotting position (nonparametric method).
- b) The city decides to build a flood levee for a design life of 30 years. The *risk of failure* that they are willing to accept during the design life is 1 chance in 5 (or 0.20). The city should design the levee for a _____-year return period flood, which has an estimated discharge of _____ cfs based on a fitted EVI distribution.

a) Parametric

$$\hat{p} = P\{X \geq 4000\} = 1 - P\{X < 4000\} = 1 - \hat{F}(4000)$$

$$= 1 - \exp\left[-\exp\left(-\left\{\frac{4000 - 1203.6}{867.0}\right\}\right)\right]$$

$$= 1 - 0.96104 = 0.03896$$

$$\hat{T} = 1/\hat{p} = 1/0.03896 = 25.7 \text{ yr}$$

Nonparametric

$$\hat{p} = P(X \geq X_{(m)}) = \frac{m}{N+1} \quad \frac{1}{T} = \frac{N+1}{m} = \frac{60+1}{3} = 20.3 \text{ yr}$$

$$b) R = 1 - (1-p)^m$$

$$1-R = (1-p)^m$$

$$(1-R)^{1/m} = 1-p$$

$$p = 1 - (1-R)^{1/m} = 1 - (1-0.20)^{1/30}$$
$$= 0.00741$$

$$T = 1/p = 1/0.00741 = 134.9 \text{ yr}$$

$$\hat{Q}(p) = 1203.6 - 867 \ln(-\ln(1-0.00741))$$
$$= 5453 \text{ cfs}$$